

Due 10/05/09

EE6311 Fall 2009 Homework #3  
Introduction to AWR Microwave Office or Agilent ADS  
Transmission Lines

If designing in AWR:

- Read the AWR introduction "Getting Started (this version is 2004)," specifically:
- #3. AWR Design Environment Suite Section; review the Basic Operations sections
- #4 MWO: Using the Linear Simulator; read and perform the tasks outlined in the "Creating a Lumped Element Filter" project.
- Print out your final filter design example and response.

OR

If designing in Agilent ADS:

- Watch the ADS movies on the following site:  
<http://ece-classweb.ucsd.edu/fall07/ece166/>.  
ADS Tutorials
  - Watch ADS example 1: \*.wmv file ~ 4 minutes, OR
  - Read ADS tutorial and/or Basics of ADS
- Using the elements from the #4 MWO: "Creating a Lumped Element Filter" project, design the project in ADS
- Print out your final filter design example and response.

-----  
For the following transmission lines, design each network "on paper" first using the graphical method. You will be determining the required width of the center conductor to give you the impedance value required. Then use MWO or ADS to simulate the TML. Submit your final circuit schematic and frequency (2 – 15 GHz) response plots (on the same graph of  $|S_{21}|$  in dB,  $|S_{11}|$  in dB) for each design.

Use: Center frequency,  $f_0 = 10$  GHz for all designs  
Port impedances =  $50 \Omega$  unless specified otherwise  
substrate  $\epsilon_r = 2.2$   
substrate thickness,  $h = 0.381$  mm for microstrip,  $b = 0.762$  mm for stripline,  $h = 1$  mm for CPW  
conductor thickness =  $10 \mu\text{m}$   
conductor metal = Au (use default value for rho in AWR or ADS)

1. Determine the appropriate line widths for microstrip transmission lines with the following characteristic impedances: Use an empirical or graphical method to compute line widths and then use AWR TxLine or Agilent Linecalc to compare.

- $Z_0 = 35 \Omega$ , place quarter-wave transformers on each side to match the line impedance to the port impedance
- $Z_0 = 50 \Omega$
- $Z_0 = 150 \Omega$ , place quarter-wave transformers on each side to match the line impedance to the port impedance, for this case, plot  $|S_{11}|$  on the Smith Chart

2. Repeat problem 1 for stripline transmission media.

# Homework #3

## Design of transmission lines

$$f = 10 \text{ GHz}$$

Microstrip (a)  $Z_0 = 35 \Omega$

(b)  $Z_0 = 50 \Omega$

(c)  $Z_0 = 150 \Omega$

$$\epsilon_r = 2.2$$

$$h = 381 \mu\text{m}$$

$$35 \Omega \quad \frac{W}{h} \approx 5 \Rightarrow W = 1.905 \text{ mm}$$

$$50 \Omega \quad \frac{W}{h} \approx 2.9 \Rightarrow W = 1.105 \text{ mm}$$

$$150 \Omega \quad \frac{W}{h} \approx 0.28 \Rightarrow W = 0.107 \text{ mm}$$

$$Z_{\text{trans}} = \sqrt{(35)(50)} = 41.83 \Omega \quad \epsilon_{\text{eff}} = 1.8$$

$$Z_{\text{trans}} = \sqrt{(50)(150)} = 86.6 \Omega \quad \epsilon_{\text{eff}} = 1.8$$

u strip

$$41.83 \Omega; \frac{W}{h} \approx 3.2 \Rightarrow W \approx 1.22 \text{ mm}$$

$$86.6 \Omega; \frac{W}{h} \approx 1.4 \Rightarrow W \approx 0.533 \text{ mm}$$

$$\lambda/4 = \frac{c}{f \sqrt{\epsilon_{\text{eff}}}} = 0.559 \text{ cm}$$

Stripline (a)  $Z_0 = 35 \Omega$

(b)  $Z_0 = 50 \Omega$

(c)  $Z_0 = 150 \Omega$

$$\epsilon_r = 2.2$$

$$h = 0.762 \text{ mm}$$

$$\sqrt{\epsilon_r Z_0} = 51.91 \quad W/b \approx 1.6 \Rightarrow W = 1.22 \text{ mm}$$

$$\sqrt{\epsilon_r Z_0} = 74.2 \quad W/b \approx 0.9; W = 0.69 \text{ mm}$$

$$\sqrt{\epsilon_r Z_0} = 222 \quad \frac{W}{b} \approx 0.08; W \approx 0.061 \text{ mm}$$

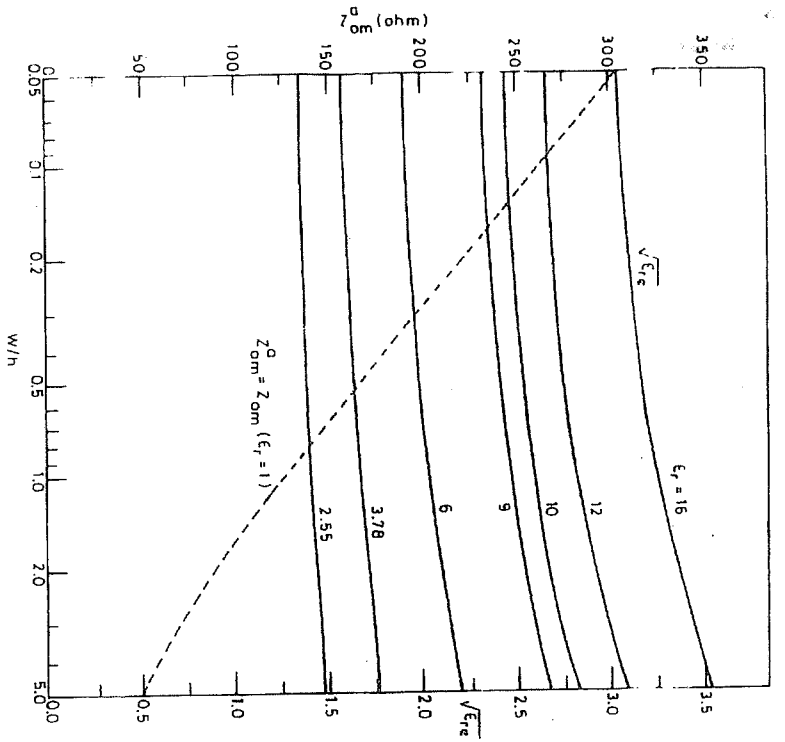
$$\sqrt{\epsilon_r Z_0} = 62.0 \quad \frac{W}{b} \approx 1.2 \Rightarrow W \approx 0.914 \text{ mm}$$

$$\sqrt{\epsilon_r Z_0} = 128 \quad \frac{W}{b} \approx 0.3 \Rightarrow W = 0.229 \text{ mm}$$

$$\lambda = \frac{c}{f \sqrt{\epsilon_r}} = \frac{3 \times 10^{10} \text{ cm/s}}{10 \times 10^9 \sqrt{2.2}} = 2.02 \text{ cm}$$

$$\lambda/4 = 0.505 \text{ cm}$$

as Figure 2.8. Here  $\epsilon_{re}$  is the same as  $\epsilon_{eff}$  above.



*whereas for microstrip*

In this figure the value of  $\sqrt{\epsilon_{re}}$  is plotted as a function of  $W/h$  for various values of the substrate dielectric constant  $\epsilon_r$ . The variation of characteristic impedance for air microstrip ( $Z_{0m}^A$  or  $\epsilon_r = 1$ ) is also shown by the dotted curve. The impedance for any value of  $\epsilon_r$  can be obtained by dividing  $Z_{0m}^A$  by the corresponding value of  $\sqrt{\epsilon_{re}}$ . It may be seen from Figure 2.8 that the impedance value decreases when the strip width to substrate height ratio ( $W/h$ ) is increased, since an increase in  $W$  (or decrease in  $h$ ) increases the line capacitance.

Since the guided wavelength in the microstrip  $\lambda_g$  is related to  $\epsilon_{re}$  by the expression

$$\lambda_g = \frac{\lambda_0}{\sqrt{\epsilon_{re}}} \quad (2.30)$$

and  $\epsilon_r$  values. The parameter range of  $w/h$  and  $\epsilon_r$  is chosen such that it spans the domain of typically encountered, practical values.

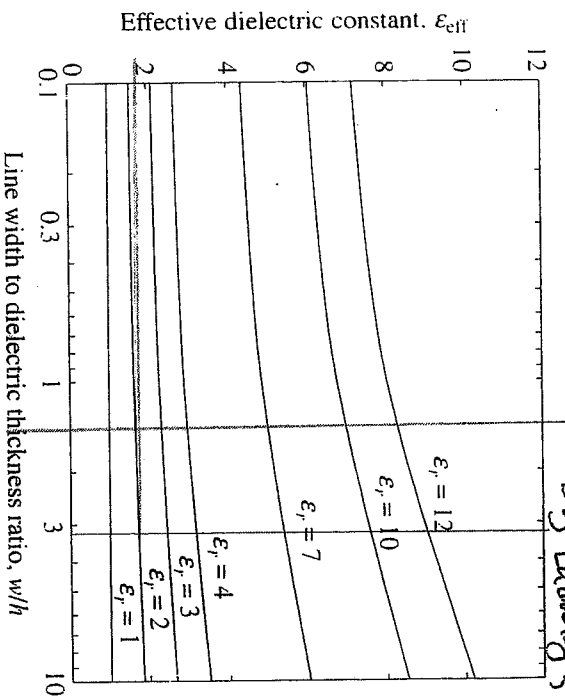


Figure 2-21 Effective dielectric constant of the microstrip line as a function of  $w/h$  for different dielectric constants.

*From RF-IC Design MEd  
by Ludwig & Bogdanov*

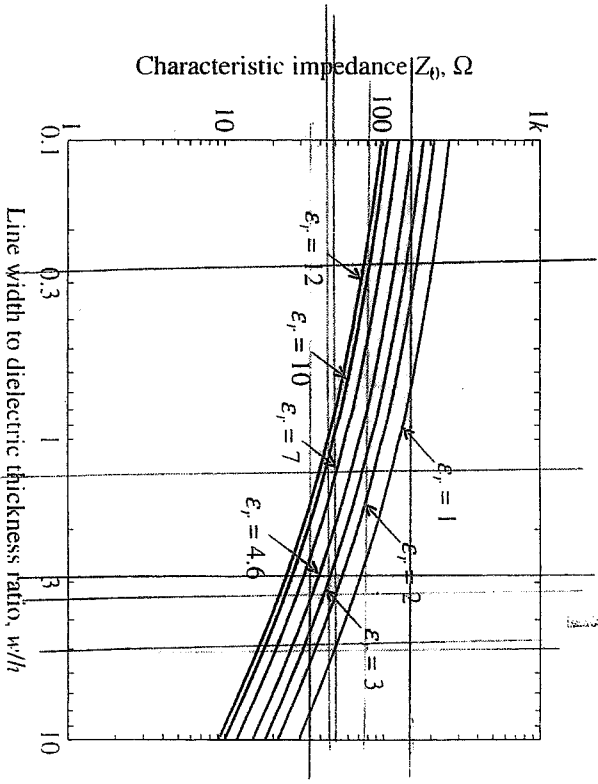


Figure 2-20 Microstrip characteristic impedance as a function of  $w/h$

If the strip width is wide enough so that the fringe fields do not interact, i.e.:  $w/b$  greater than or equal to 0.35, then another relation is applicable

$$Z_0 \sqrt{\epsilon} = \frac{94.15}{\left( \frac{w/b}{1-t/b} + \frac{C_f'}{0.0885 \epsilon_R} \right)} \quad (2.4)$$

where,

$$C_f' = \frac{0.0885 \epsilon}{\pi} \left[ \frac{2}{1-t/b} \log_e \left( \frac{1}{1-t/b} + 1 \right) - \left( \frac{1}{1-t/b} - 1 \right) \log_e \left( \frac{1}{(1-t/b)^2} - 1 \right) \right] \text{ Pf/cm} \quad (2.5)$$

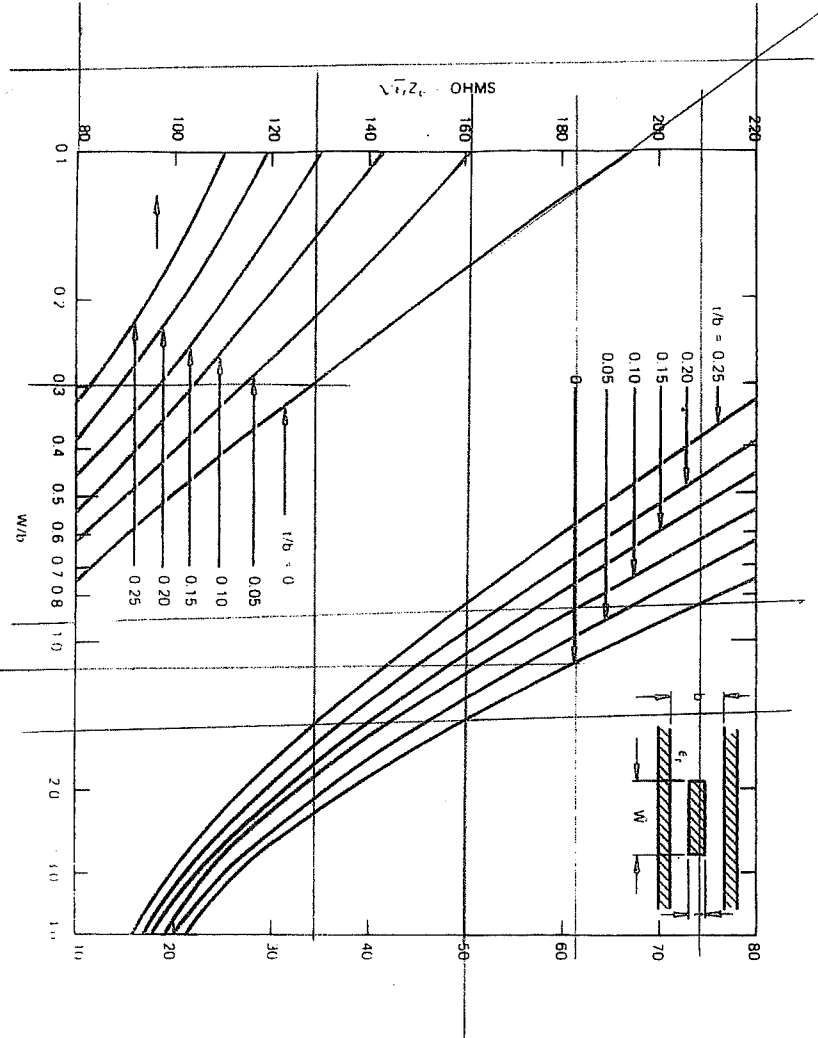


FIG. 2-3 General Curves for Characteristic Impedance of Dielectrically Loaded Stripline

Stripline ckt Design by Hanken House Jr, 1975

and

$$Z_{ocp} = \frac{1}{C V_{cp}} = \frac{30\pi}{\sqrt{\epsilon_r + 1}} \frac{K'(k)}{K(k)} \quad (\text{ohm}) \quad (7.6)$$

where  $c$  is the velocity of electromagnetic waves in free space. Values of characteristic impedance  $Z_{ocp}$  computed from Equation (7.6) are shown in Figure 7.4. Measured values of  $Z_{ocp}$  for  $\epsilon_r = 9.6, 16$  and  $130$

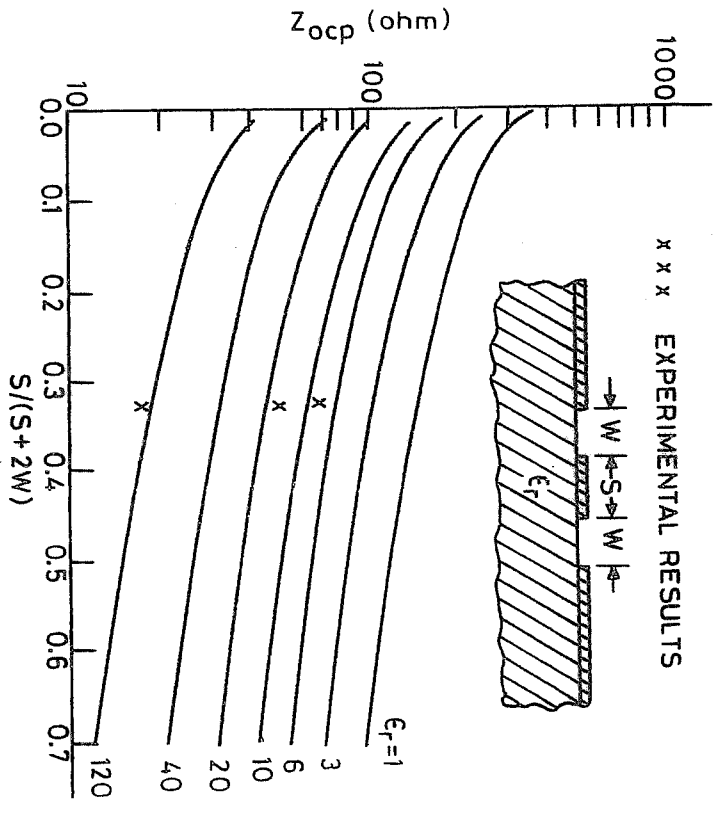


Figure 7.4 Characteristic Impedance of Coplanar Waveguides (from [1])

are also shown in this figure. Wen [1] points out that  $Z_{ocp}$  increases by less than 10 percent, for large values of  $\epsilon_r$ , when the thickness of the substrate is reduced from infinite to  $w$ , the width of the slots (that is, when  $W/h \rightarrow 1$ ).

Microstrip lines & slotlines K Gupta